

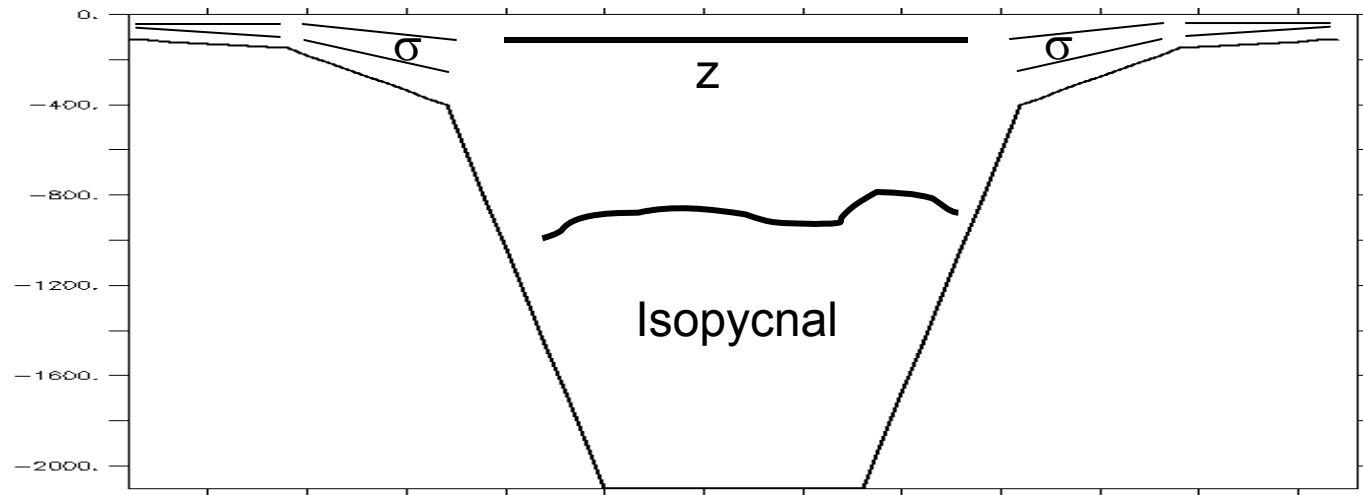
TESTING
of the PRESSURE GRADIENT
ERROR
in a
TERRAIN-FOLLOWING HYCOM

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Hybrid coordinates: isopycnal, z, sigma

- Z : upper layers, unstratified seas
- Isopycnal : stratified deep ocean (conserve water mass property)
- σ (terrain-following) : coastal areas, shelves and top of continental slopes



Parametrization of coordinates

Choice of coordinates	n _{hybrid}	Number of hybrid layer (z+σ)
	n _{sigma}	Number of σ layer
Z-layers spacing parameter	Δp ₀₀	Thickness of the surface layer
	Δp _{00f}	Stretching factor
	Δp _{00x}	Maximum thickness
	$\Delta p(k) = \Delta p_{00} * \Delta p_{00f}^{k-1}$	
σ-layers spacing parameter	Δs ₀₀	Thickness of the surface layer
	Δs _{00f}	Stretching factor
	Δs _{00x}	Maximum thickness
	$\Delta s(k) = \Delta s_{00} * \Delta s_{00f}^{k-1}$	

Target densities

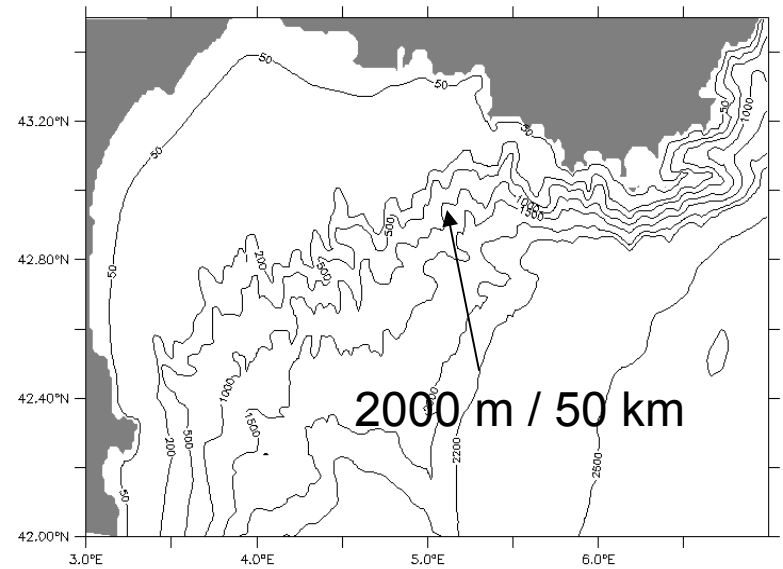
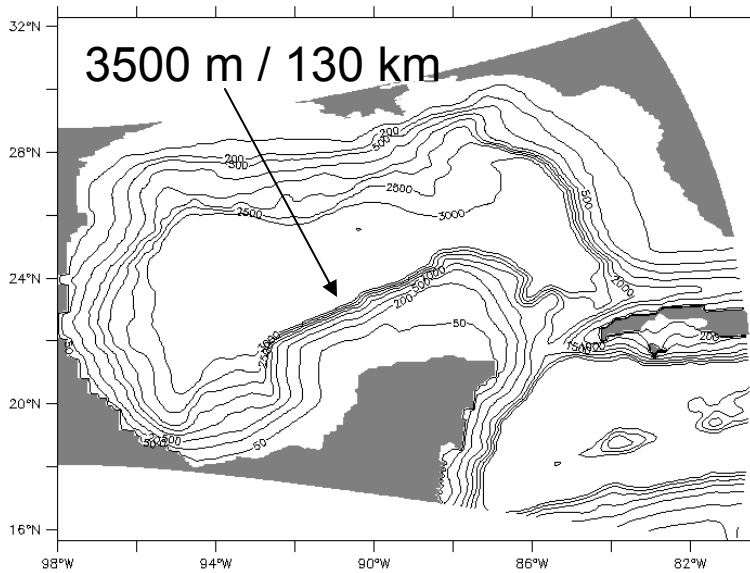
Condition : Δs₀₀, Δs_{00f}, Δs_{00x} ≤ Δp₀₀, Δp_{00f}, Δp_{00x}

$$\Delta h = \min (\Delta h_z , \max (\Delta h_s, \text{depth}/n_{\text{sigma}}))$$

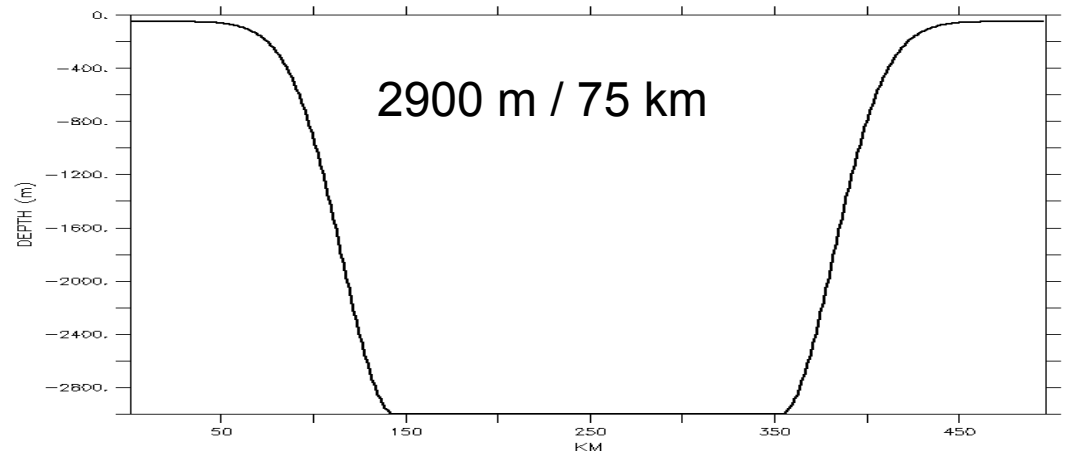
Deep ocean ↗
Very shallow water

↖ Coastal area

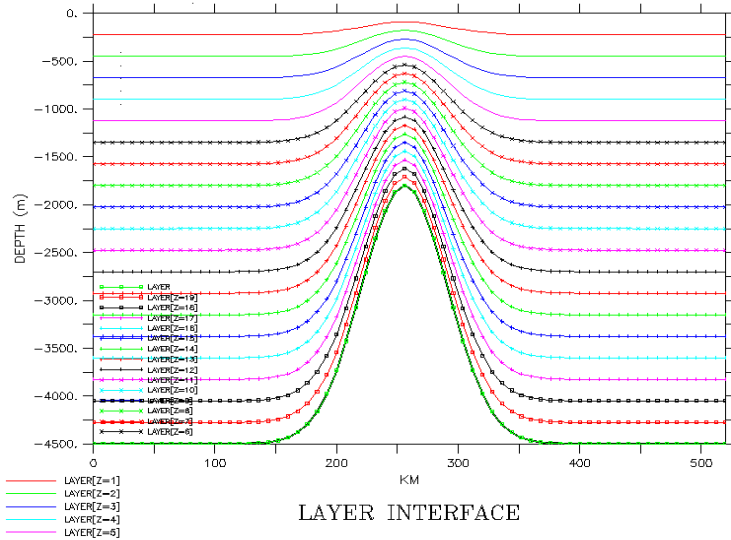
How does HYCOM perform over steep continental rises ?



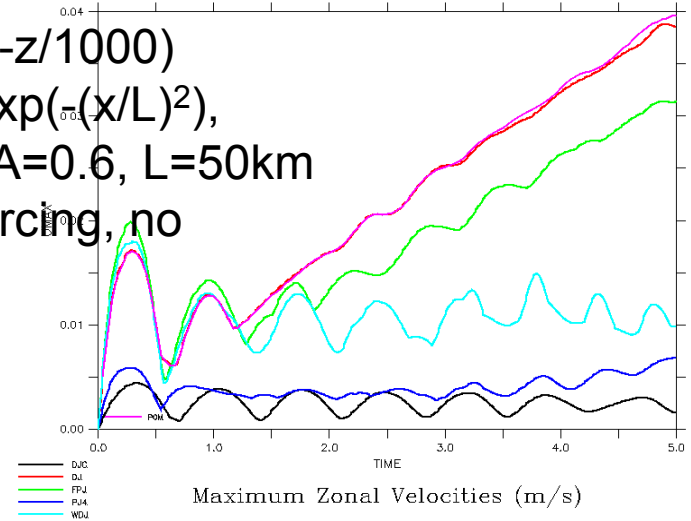
Realistic but extremely steep continental slope :
 $H=50+2950*\exp(-(x/L)^2)$,
 $L=40$ km



σ -models and the seamount problem



$T=5+15 \exp(-z/1000)$
 $H=H_0 (1-A \exp(-(x/L)^2))$,
 $H_0=4500\text{m}$, $A=0.6$, $L=50\text{km}$
 At rest, no forcing, no
 viscosity...



Irrelevant case for HYCOM

- never pure σ -layer mode,
- σ -layers over shelf,
- isopycnal layer in deep layers

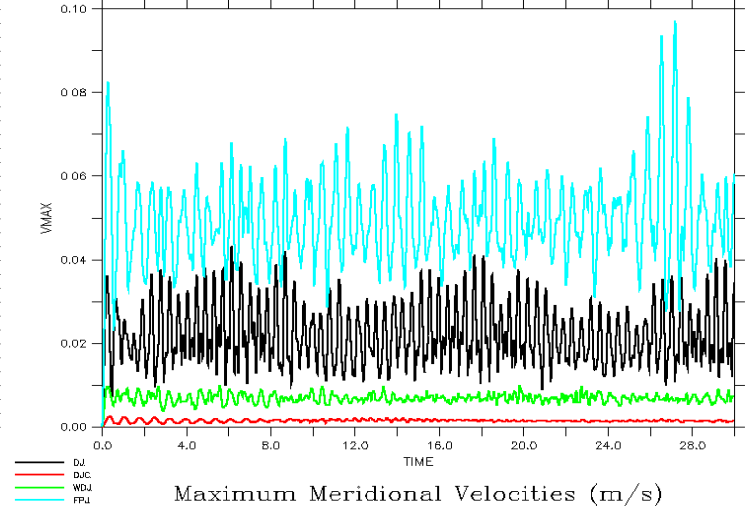
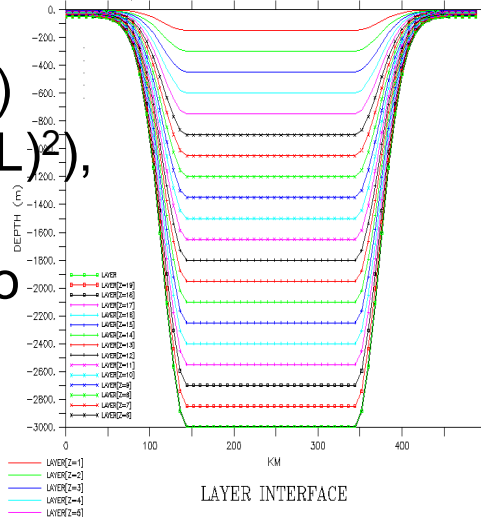
No Pressure Gradient Error (PGE) with z and isopycnal layers

HYCOM
 $V_{\max}=2.62 \text{ m/s} !$

PGE with σ -layers over shelf ?

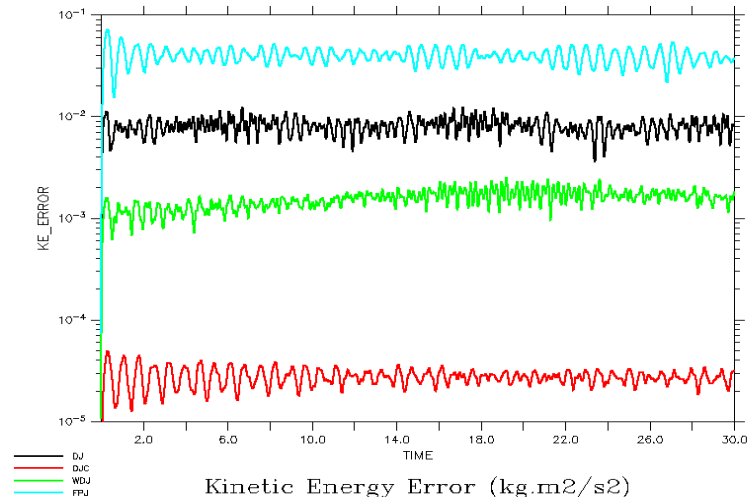
ROMS

$T=5+15 \exp(-z/1000)$
 $H=50+2950 \cdot \exp(-(x/L)^2)$,
 $L=40 \text{ km}$
 At rest, no forcing, no
 viscosity...



Accuracy of Pressure gradient schemes

1. DJC density Jacobian using monotized cubic polynomial fits
2. WDJ Weighted density Jacobian
3. DJ standard Density Jacobian
4. FPJ Finite-Volume Pressure Jacobian



PGE with σ -layers over shelf ?

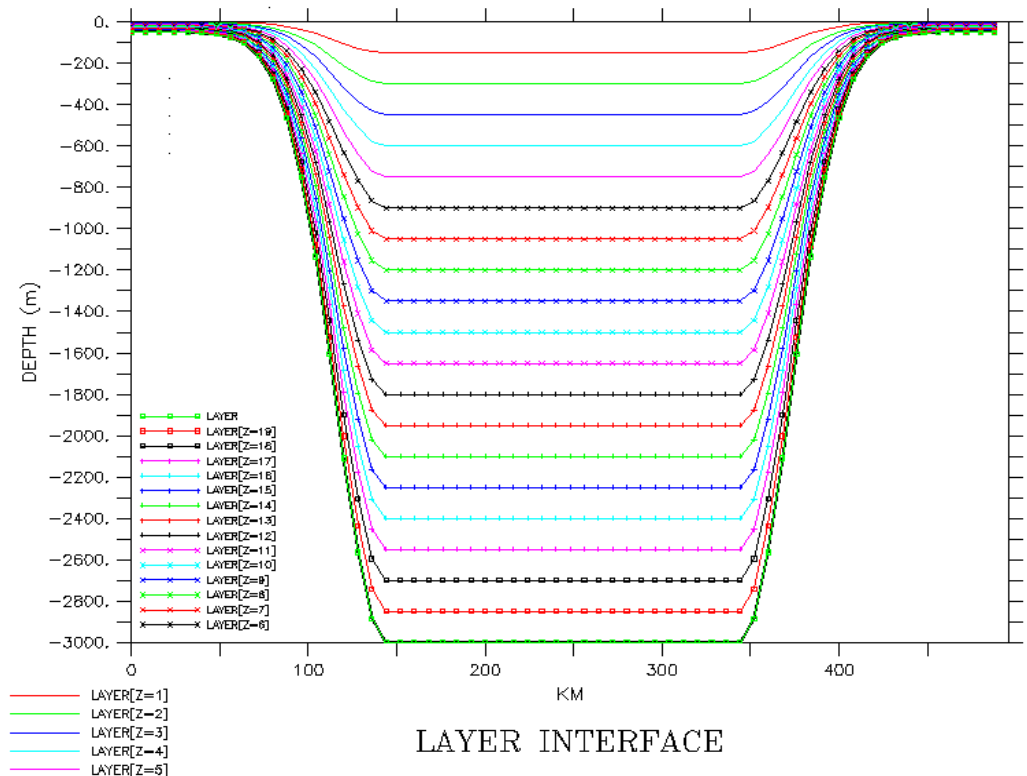
HYCOM

$$T=5+15 \exp(-z/1000)$$

$$H=50+2950 \cdot \exp(-(x/L)^2),$$

$$L=40 \text{ km}$$

At rest, no forcing, no
viscosity, no diffusivity, no
bottom friction...



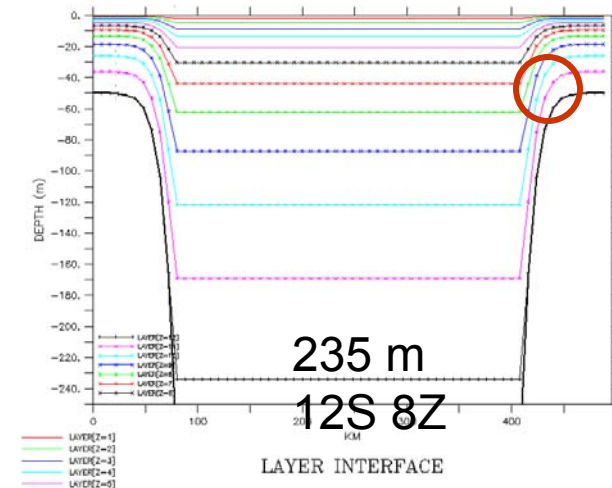
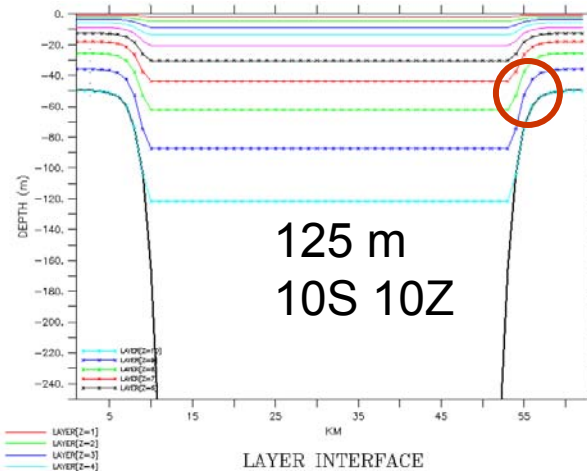
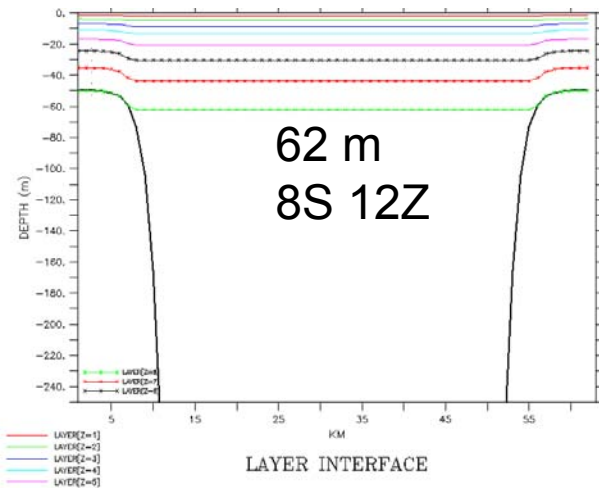
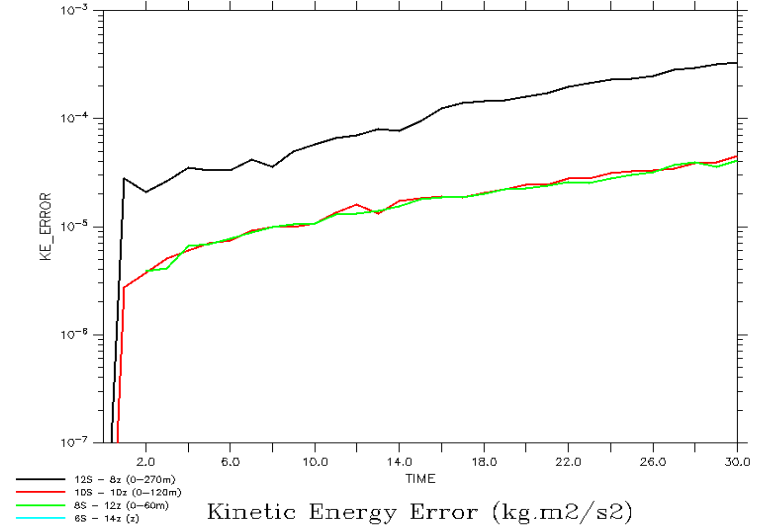
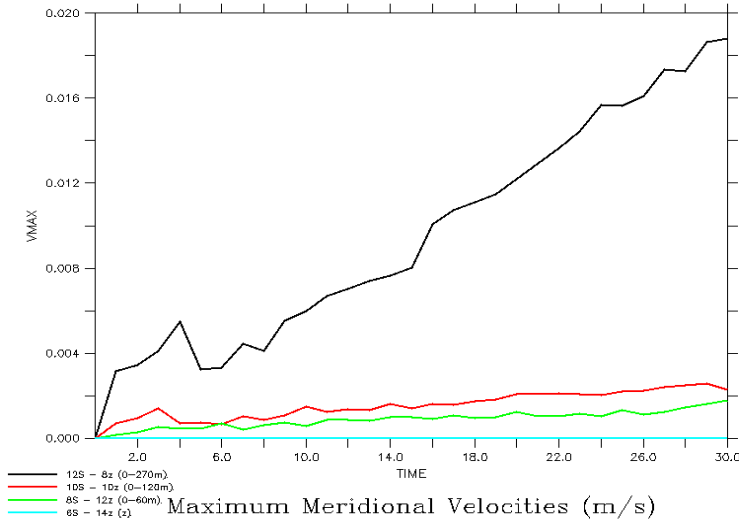
Blows up, but irrelevant case...

How deep can we use σ -layers ?

$$\Delta p_{00} = \Delta s_{00} = 2$$

$$\Delta p_{00f} = \Delta s_{00f} = 1.37$$

HYCOM



Conclusion

- Numerical experiments explore the limitation of the use of σ -layers in HYCOM. In case of an extremely steep slope, limitations come from computational errors in both terms of the horizontal pressure gradient formulation:

$$\alpha \delta_z p = \delta_s M - p \delta_s \alpha$$

- Pressure gradient errors are estimated as motion induced in an ocean initially at rest, uniformly stratified and unforced
- Pressure gradient errors can occur with the use of σ -layers, only
- Pressure gradient scheme is clearly less efficient in HYCOM than in pure σ -models (ROMS-POM)

Conclusion

- However the use of a combination of hybrid coordinates mitigate inaccuracy in horizontal pressure gradient term
- Careful choice of σ -layer parametrization should not induce any perturbation of the circulation due to PGE:
 - HYCOM performs **accurately over shelves** where slopes are gentle. In such conditions, **PGE are comparable with σ -models** (a few mm/s)
- Careful choice : do not use σ -layers above steep slopes

Perspectives

- In HYCOM, the use of σ -layers over shelf breaks requires improvements in the pressure gradient scheme
- Two approaches:
 - Density Jacobian formulation ?
 - More accurate Pressure Jacobian : cubic formulation (Shchepkin & Mc Williams, 2003) instead of the current linear scheme ?